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A Wideband Spatial Channel Model for System-Wide Simulations

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Abstract-A wideband space-time channel model is defined, which captures the multiple dependencies and variability in multicell system-wide operating environments. The model provides a unified treatment of spatial and temporal parameters, giving their statistical description and dependencies across a large geographical area for three outdoor environments pertinent to thirdgeneration cellular system simulations. Parameter values are drawn from a broad base of recently published wideband and multiple-antenna measurements. A methodology is given to generate fast-fading coefficients between a base station and a mobile user based on the summation of directional plane waves derived from the statistics of the space-time parameters. Extensions to the baseline channel model, such as polarized antennas, are given to provide a greater variety of spatial environments. Despite its comprehensive nature, the model's implementation complexity is reasonable so it can be used in simulating large-scale systems. Output statistics and capacities are used to illustrate the main characteristics of the model.

Index Terms—Angle spread, antennas, arrays, capacity, channel model, delay spread, directional, multipath channel, multipleinput multiple-output (MIMO), polarization, spatial channel model (SCM), simulations, spatial channel, stochastic model, time-varying channel, wideband.

I. INTRODUCTION

T HE INTRODUCTION of multiple antennas in the thirdgeneration cellular systems requires the detailed modeling of the spatial characteristics of the channel environment. Thus, the existing, widely used industry-standardized temporal-only channel models [1]–[3] need to be extended so as to properly

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include the spatial domain. In the meantime, there has been a considerable number of publications on the topic of multipleinput multiple-output (MIMO) channel models. These can be grouped into two categories: 1) physical or scatterer-based models, which model the directional properties of the multipath components at the transmitter and receiver; 2) nonphysical or correlation-based models, which model the transfer functions from each transmit to each receive antenna element, and the correlations between them.

In the first category, one can distinguish between 1) generalizations of the tapped-delay-line and related approaches [4]–[11], which define the angular and delay distribution of radiation, and 2) geometry-based stochastic models, which model the spatial distribution of scatterers and reflectors [12]–[20].

The nonphysical models focus on the signal correlations at different antenna elements and typically assume correlated complex Gaussian fading. For different types of channels and complexity requirements, various models have been proposed, where the correlation matrix is 1) the identity matrix [21], [22], 2) separable between transmitter and receiver [23]–[28], and 3) a more general nonseparable matrix with a particular approach of its representation as an eigenmode expansion, where the eigenspaces are identical at transmitter and receiver, is treated in [29].

The above-cited papers predominantly concentrate on flatfading MIMO channels with no large-scale changes. The only existing comprehensive MIMO channel model, also formally defined by a cooperative effort of industry and academia, is the COST259 Directional Channel Model [30]–[33]. This model is very detailed, and thus also rather complicated. In particular, this model 1) is a comprehensive model covering all kinds of radio environments; 2) allows for the simulation of continuous large-scale changes of the mobile-station position; 3) is intended to be system-independent, i.e., to work for different carrier frequencies, and different system bandwidths. For that reason, it specifies a time- and angle continuous model. Also, a standardized model for indoor MIMO communications was recently finalized [34].

In [35], a hybrid model has been proposed to represent a general MIMO channel using a hybrid representation of the angular spectrum at the mobile and correlated fading at the base, once second-order statistics, such as power delay and angular spectra are specified. The current work represents the MIMO channel as a superposition of clustered constituents, with stochastic powers, angles of departure (AoD) and arrival (AoA), as well as times of arrival. Recommendations are made

here on generation of second-order statistical parameters based on both original and published results.

The industry consortia that develop the third-generation standards [third-generation partnership project (3GPP) and 3GPP2] require the definition of widely accepted frameworks (e.g., channel environments and assumptions) on which to evaluate the proposed technologies. The work presented in this paper is the culmination of a joint effort by 3GPP and 3GPP2. The two standards bodies mandated the extension of the existing industry-adopted temporal models to provide a framework for a wideband multiantenna system-wide simulation analysis. The finalized and adopted specification is described in [36].

The proposed model is intended for the three most common cellular environments (as decided by the two standards bodies): suburban macrocells, urban macrocells, and urban microcells. The timeframe of the intended system simulations is assumed short enough, so that the model does not need to consider macroscopic terminal movement. The model is parameterized by the system bandwidth and is designed for bandwidths up to 5 MHz. Therefore, it is valid for most third-generation systems, and it allows for performance comparisons between systems using different bandwidths. Furthermore, the channel model is specifically designed for multiple-antenna architectures at the base-station (BS) and/or at the mobile station (MS). Its herein description assumes linear antenna arrays, however it is straightforward to extend it to accommodate arbitrary array topologies. Finally, its structure seeks a balance between the realistic spatial environments and modeling complexity. Specifically, it generates a set of paths with discrete angles and delays. The generation of the channel coefficients for a system-level simulation is modular in structure and effort has been made to maintain a manageable computational complexity.

The rest of this paper is organized as follows: Section II describes the general structure of the model by means of definitions for the operating environment, the pathloss, and the correlation between the spatial parameters from different BSs, as well as generation of fast fading coefficients. In Section III, three extensions to the baseline channel model, and a model for polarized antennas, are given to represent a greater variety of common spatial environments. Finally, Section IV provides output statistics of the model and gives some insight into its behavior in terms of MIMO capacity metrics.

II. GENERAL STRUCTURE OF CHANNEL MODEL

This section describes the baseline spatial channel model and its implementation. The purpose of the model is to generate the channel coefficients between a given BS and mobile terminal (MS) based on a set of spatiotemporal parameters.

The statistical nature of the model is a feature that makes it particularly suitable for system-level analysis. The first step in the model is to choose one of three channel scenarios as described in Section II-A. Mobile users (MS) are dropped randomly in the area to be simulated. Note that in an actual system simulation, a large number of BSs and MSs may be modeled. However, in describing the proposed channel model, we focus on a single BS/MS pair. Every BS–MS pair is a different realization of the channel conditions drawn from a common, system-wide, distribution. The model defines interactions of many BSs and many sectors to an MS using the site-to-site shadowing correlation. It does not define methods to model intercell interference since this is more of a simulation methodology issue than a channel model definition issue. Nevertheless the model defines all the necessary channel effects that would be needed for modeling intercell interference. Also, the model does not define channel model dependencies between MSs. Although correlation between MSs do exist (e.g., when MSs are colocated) the model does not include them since it would make the model less flexible. However, it is possible for the reader to add this functionality to the current channel model without violating any of the model's design approaches. The relationship between a given channel scenario and the channel coefficients for a BS/MS pair can be described in terms of three levels of abstraction.

At the macroscopic level, time-averaged local properties of the channel are described, e.g., the average power, delay spread (DS), and angle spread (AS). These quantities are also designated as "composite" parameters to imply the inclusion of all delayed components. Apart from a deterministic part, these variables have a log-normal random part, which captures the fluctuations due to propagation through several independent "city block" regions. These features are described in Section II-C and D.

Focusing in to a deeper "mesoscopic" level, the channel has additional structure (see Section II-E). In particular, each composite energy cluster is decomposed into multiple paths with relative delays, and AoA and AoD consistent with the composite statistics. Each of these paths can be thought of as coming from different buildings within the neighborhood of that block. Note that the above naming convention (AoD/AoA) corresponds to downlink channels, for signals originating at the BS and terminating at the MS. However, the full model is applicable also for uplink channels. Also at this mesoscopic level, the path delays and average path powers are generated as realizations of random variables. This is in contrast to the commonly used ITU models for link-level simulations (e.g., Pedestrian A or Vehicular A models, [1]) where these parameters are fixed. The proposed model is particularly well suited for system-level analysis because its statistical nature more accurately reflects the wide range of user parameters found in actual systems.

At the deepest, microscopic level, each of these paths undergoes Rayleigh fading, generated from the temporal variability of the particular link (e.g., due to the terminal's movement). Each path is represented as a sum of subpaths modeled as planewaves (see Section II-F).

Since the various length-scales are not always clearly separable, the interpretation of these levels of abstraction does not always correspond with reality. However, they certainly make sense and can always be used to describe the experimental data of outdoors channels.

A. Choosing a Channel Scenario

First, a channel scenario is chosen, which defines a specific set of typical physical parameters of the environment. As

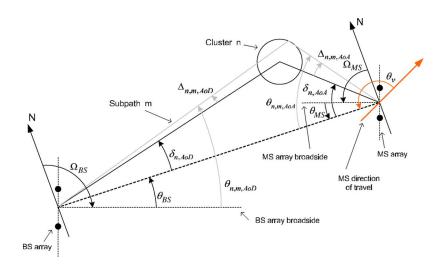


Fig. 1. Angular variables definitions.

mentioned in Section I, the analysis is limited to three general channel scenarios.

1) Suburban Macro: The suburban macrocell scenario describes a rural/suburban area with generally residential buildings and structures. The vegetation and any hills in the area are also assumed not to be too high. The BS antenna position is high, well above local clutter. As a result, the AS and DS are relatively small. In addition, the base-to-base distance is approximately 3 km.

2) Urban Macro: The urban macrocellular environment describes large cells in areas with urban buildings of moderate heights in the vicinity and significant scattering. The BS antennas are placed at high elevations, well above the rooftops of any buildings in the immediate vicinity. The distance between BSs is again about 3 km. This scenario assumes moderate to high ASs at the BS and also large DSs.

In urban environments, street canyon effects, i.e., wave propagation down relatively narrow streets with high buildings on both sides may be important in some cases and depending on their probability of occurrence, may lead to deviations from the generic urban macrocell case. Thus, street canyon effects are treated as optional extensions to the urban macroscenario. Details are discussed in Section III-C.

Another important effect, also treated as an option in this scenario, is the existence of additional clusters of energy due to far scatterers originating from high buildings. This is discussed in Section III-A.

3) Urban Micro: In contrast to the above scenario, the urban microcell scenario describes small urban cells with interbase distances of approximately 1 km. Base antennas are located at rooftop level and therefore large ASs are expected at the BS, even though the DS is only moderate.

In the case of macrocell scenarios discussed above, due to the relatively large area allocated to each BS, the fraction of locations in the cell with the chance to have a line-of-sight (LOS) component from the BS is small. Thus, for simplicity such channels are not modeled in the macrocell cases. However, for smaller cells, as in the case of microcell scenario, the users with LOS components cannot always be neglected. Thus, the way of including them is analyzed in Section III-B.

B. Dropping Users

Once the scenario has been chosen and the locations of the $N_{\rm BS}$ BSs with the desired geometry and interbase distances have been determined, one may start instantiating users in the area of interest. This entails first randomly generating the user locations. In addition, one needs to specify other user-specific quantities, such as their velocity vector **v**, with its direction θ_v drawn from a uniform [0, 360°) distribution. Also, the specifics of the MS antenna or antenna array have to be determined, such as array orientation, $\Omega_{\rm MS}$, also drawn from a uniform [0, 360°) distribution, polarization, etc. Fig. 1 illustrates the various angle definitions.

It should be stressed that while the velocity of a particular MS is generally assumed to be nonzero, it is assumed here that the macroscopic and mesoscopic parameters do not vary over the duration of a simulation run. However, the velocity and position of the MS directly affects the microscopic parameters (e.g., the channel coefficients) as seen in Section II-F. This assumption does not allow the model to accurately treat the behavior of some users over the duration of a simulation (~minutes), since it does not describe dynamical hand-off situations or the passage of a particular user through different shadowing regions. However, it is expected that the statistics at a system level will not be affected.

C. Pathloss

The following two pathloss models come from the widely accepted COST 231 models [37]. For a given user, the pathloss is a fixed multiplicative factor which is applied to all N multipath components described in Section II-E.

1) Suburban Macrocell and Urban Macrocell Environments: The macrocell pathloss is chosen to be the modified COST231 Hata urban propagation model, given in [37, eq. (4.4.1)]

$$PL[dB] = (44.9 - 6.55 \log_{10}(h_{BS})) \log_{10} \left(\frac{d}{1000}\right) + 45.5 + (35.46 - 1.1h_{MS}) \log_{10}(f_{c}) - 13.82 \log_{10}(h_{MS}) + 0.7h_{MS} + C$$
(1)

where $h_{\rm BS}$ is the BS antenna height in meters, $h_{\rm MS}$ the MS antenna height in meters, $f_{\rm c}$ the carrier frequency in megahertz, d is the distance between the BS and MS in meters, and C is a constant factor (C = 0 dB for suburban macro and C = 3 dB for urban macro).

Setting these parameters to $h_{\rm BS} = 32 \text{ m}$, $h_{\rm MS} = 1.5 \text{ m}$, and $f_{\rm c} = 1900 \text{ MHz}$, the pathloss formulas for the suburban and urban macroenvironments become, respectively, $\rm PL = 31.5 + 35 \log_{10}(d)$ and $\rm PL = 34.5 + 35 \log_{10}(d)$. The distance d is required to be at least 35 m.

2) Microcell Environment: The microcell non-LOS (NLOS) pathloss is chosen to be the COST 231 Walfish–Ikegami NLOS model, [37, eqs. (4.4.6)–(4.4.16)], with the following parameters: BS antenna height $h_{\rm BS} = 12.5$ m, building height 12 m, building-to-building distance 50 m, street width 25 m, MS antenna height 1.5 m, orientation 30° for all paths, and selection of metropolitan center. With these parameters, the pathloss formula simplifies to

$$PL[dB] = -55.9 + 38 \log_{10}(d) + \left(24.5 + \frac{f_c}{616.67}\right) \log_{10}(f_c).$$
(2)

The resulting pathloss at 1900 MHz is $PL(dB) = 34.53 + 38 \log_{10}(d)$, where *d* is in meters. The distance *d* is assumed to be at least 20 m. It may be noted that the pathloss models adopted for the microcell and macrocell environments are quite similar for the parameters described above. A bulk log-normal shadowing applying to all subpaths has a standard deviation of 10 dB. The microcell LOS pathloss is based on the COST 231 street canyon model, given in [37, eq. (4.4.5)]

$$PL[dB] = -35.4 + 26 \log_{10}(d) + 20 \log_{10}(f_c).$$
(3)

The resulting pathloss at 1900 MHz is $PL[dB] = 30.18 + 26 \log_{10}(d)$, with f_c in megahertz and d in meters and $d \ge 20$ m. Log-normal shadowing applied to all subpaths has a standard deviation of 4 dB.

D. Generation of Other Composite Parameters

In this section, the generation of shadowing coefficients is described, as well as the composite AS and DS and their cross correlations. These will then be used in Section II-E to generate the mean AoD and relative delays of the intracluster subpaths.

1) Composite Parameters for Macrocell Environments: The details of the generation of shadow-fading, AS and DS for the case of macrocell environments are described in this section.

Shadow-fading fluctuations of the average received power are known to be log-normally distributed. Recently, for macrocell scenarios, the fluctuations in delay and AS were shown to behave similarly, [38]–[40]. The reason is that these quantities are sums of powers of individual subpaths times the square of their corresponding delay times or angles. Since the powers are log-normally distributed and sums of log-normal variables are (approximately) log-normal [41], this implies that ASs and DSs have log-normal distributions. This explanation of the observed lognormal behavior of the DS was first conjectured in [38]. This motivation of how AS and DS are lognormally distributed also suggests that they will be correlated with shadow fading and each other.

Based on this log-normal behavior, the DS $\sigma_{DS,n}$, BS AS $\sigma_{AS,n}$ and shadow fading $\sigma_{SF,n}$ parameters of the signal from BS *n*, where $n = 1, ..., N_{BS}$, to a given user can be written as

$$10\log_{10}(\sigma_{\mathrm{DS},n}) = \mu_{\mathrm{DS}} + \epsilon_{\mathrm{DS}}X_{1n} \tag{4}$$

$$10\log_{10}(\sigma_{\mathrm{AS},n}) = \mu_{\mathrm{AS}} + \epsilon_{\mathrm{AS}} X_{2n} \tag{5}$$

$$10\log_{10}(\sigma_{\mathrm{SF},n}) = \epsilon_{\mathrm{SF}} X_{3n}.$$
 (6)

In the above equations X_{1n} , X_{2n} , and X_{3n} are zero-mean, unitvariance Gaussian random variables. $\mu_{\rm DS}$ and $\mu_{\rm AS}$ represent the median of the DS and ASs in decibels. Similarly, the ϵ -coefficients are constants representing the log-normal variance of each parameter (e.g., $\epsilon_{\rm DS}^2 = E[(10 \log_{10}(\sigma_{\rm DS,n}) - \mu_{\rm DS})^2])$. The values of μ and ϵ for the two macrocell models appear in Table I. While there is some evidence [38], [39] that delay and AS may depend on distance between the transmitter and receiver, the effect on the system behavior is considered to be minor. Therefore, this dependence on the distance is not included here. Once $\sigma_{{\rm DS},n}$ and $\sigma_{{\rm AS},n}$ have been determined, they are used to generate the relative delays and mean AoD of the intracluster paths, see Section II-E.

Recent measurements have shown that for a given BS–MS pair, the various σ above are correlated [40], [42], [43]. In particular, $\sigma_{SF,n}$ is negatively correlated with $\sigma_{DS,n}$ and $\sigma_{AS,n}$, while the latter two have positive correlations with each other. It should be noted that this relationship does not hold for the AS at the mobile since the different paths with distinct angles do not necessarily lead to such pronounced differences in the delays. These correlations can be expressed in terms of a covariance matrix **A**, as seen in (7), whose A_{ij} component represents the correlations between X_{in} and X_{jn} , with i, j = 1, 2, 3.

Measurements of cross correlations of these parameters between different BSs are more sketchy. In particular, only correlations between shadow-fading components have been adopted [3], [44]. These correlations are assumed to be the same between any two different BSs and are denoted by ζ . For simplicity and due to lack of further data, the cross correlation matrix between the X_{in} triplet (i = 1, 2, 3) of different BSs are assumed to be given by the following matrix **B**

$$\mathbf{A} = \begin{bmatrix} 1 & \rho_{\rm DA} & \rho_{\rm DF} \\ \rho_{\rm DA} & 1 & \rho_{\rm AF} \\ \rho_{\rm DF} & \rho_{\rm AF} & 1 \end{bmatrix}$$
$$\mathbf{B} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & \zeta \end{bmatrix}$$
(7)

with B_{ij} representing the correlations between X_{in} and X_{jm} , for i, j = 1, 2, 3 and $n \neq m$. The values chosen for these parameters are summarized below

$$\rho_{\rm DA} = E[X_{1n}X_{2n}] = +0.5$$

$$\rho_{\rm DF} = E[X_{2n}X_{3n}] = -0.6$$

$$\rho_{\rm AF} = E[X_{3n}X_{1n}] = -0.6$$

$$\zeta = E[X_{3n}X_{3m}] = +0.5 \qquad n \neq m.$$

| Channel Scenario | Suburban Macro | Urban Macro | Urban Micro |
|---|---|---|---|
| Number of paths | 6 | 6 | 6 |
| Number of sub-paths (M) per-path | 20 | 20 | 20 |
| Mean RMS AS at BS | $E(\sigma_{AS}) = 5^{\circ}$ | $E(\sigma_{AS}) = 8^{\circ}, 15^{\circ}$ | NLOS: $E(\sigma_{AS}) = 19^{\circ}$ |
| AS at BS as a lognormal RV | $\mu_{AS} = 0.69$ | $8^{\circ} \ \mu_{AS} = 0.810$ | N/A |
| $\sigma_{AS} = 10^{(\epsilon_{AS} \cdot x + \mu_{AS})}$ | $\epsilon_{AS} = 0.13$ | $\epsilon_{AS} = 0.34$ | |
| $x \sim N(0, 1)$ | | $15^{\circ} \ \mu_{AS} = 1.18$ | |
| σ_{AS} in degrees | | $\epsilon_{AS} = 0.210$ | |
| $r_{AS} = \sigma_{AoD} / \sigma_{AS}$ | 1.2 | 1.3 | N/A |
| Per-path AS at BS (Fixed) | 2° | 2° | 5° (LOS and NLOS) |
| BS per-path AoD Distribution | $N(0, \sigma^2_{AoD})$ where | $N(0, \sigma^2_{AoD})$ where | $U(-40^{\circ}, 40^{\circ})$ |
| standard deviation | $\sigma_{AoD} = r_{AS} \cdot \sigma_{AS}$ | $\sigma_{AoD} = r_{AS} \cdot \sigma_{AS}$ | |
| Mean RMS AS at MS | $E(\sigma_{AS,MS}) = 68^{\circ}$ | $E(\sigma_{AS,MS}) = 68^{\circ}$ | $E(\sigma_{AS,MS}) = 68^{\circ}$ |
| Per-path AS at MS (Fixed) | 35° | 35° | 35° |
| MS Per-path AoA Distribution | $N(0, \sigma^2_{AoA}(Pr))$ | $N(0, \sigma^2_{AoA}(Pr))$ | $N(0, \sigma^2_{AoA}(Pr))$ |
| Delay spread as a lognormal RV | $\mu_{DS} = -6.80$ | $\mu_{DS} = -6.18$ | N/A |
| $\sigma_{DS} = 10^{(\epsilon_{DS} \cdot x + \mu_{DS})}$ | $\epsilon_{DS} = 0.288$ | $\epsilon_{DS} = 0.18$ | |
| $x \sim N(0, 1)$ | | | |
| σ_{DS} in μ sec | | | |
| Mean total RMS Delay Spread | $E(\sigma_{DS}) = 0.17 \mu s$ | $E(\sigma_{DS}) = 0.65 \mu s$ | $E(\sigma_{DS}) = 0.251 \mu s$ (output) |
| $r_{DS} = \sigma_{delays} / \sigma_{DS}$ | 1.4 | 1.7 | N/A |
| Distribution for path delays | | | $U(0, 1.2\mu s)$ |
| Lognormal shadowing | 8dB | 8dB | NLOS: $10dB$ |
| standard deviation σ_{SF} | | | LOS: $4dB$ |
| Pathloss model (<i>dB</i>) | $31.5 + 35 \log_{10}(d)$ | $34.5 + 35 \log_{10}(d)$ | NLOS: $34.53 + 38 \log_{10}(d)$ |
| d is in meters | | | LOS: $30.18 + 26 \log_{10}(d)$ |

TABLE I Environment Parameters

For a given BS, the values of the cross correlations $\rho_{\rm DA}$, $\rho_{\rm DF}$, $\rho_{\rm AF}$ above were chosen to be the rounded average of the measured parameters in [40]. The value of ζ is the adopted value between BS shadow-fading parameters [3]. In addition, the choice of these values ensures that the triplet of X_{in} Gaussian random variables has a positive-definite covariance.

The random variables X_{in} can be generated with the above cross correlations by first generating 3 + 1 zero-mean unitvariance independent Gaussian random variables, namely Y_{in} , for i = 1, 2, 3 and $n = 1, \ldots, N_{BS}$, and Z_0 . For a given MS, all its MS–BS links use independent Y_{in} triplets, but a common realization of Z_0 . However, two different MSs should use independent Z_0 realizations. The X_{in} variables can then be written as

$$X_{in} = \sum_{j=1}^{3} C_{ij} Y_{jn} + \delta_{i3} \sqrt{\zeta} Z_0 \text{ where } \mathbf{C}^2 = \mathbf{A} - \mathbf{B} \quad (8)$$

and δ_{ij} is the Kronecker delta function. Note that since A-B is positive definite, the matrix square-root operation is well defined.

2) Composite Parameters for Urban Microcell Environment: In the case of the urban microcellular environment, the fact that the BS antennas are now positioned at roof-top level results to blurring the distinction between clusters and paths. This requires a different approach in dealing with delay and AS. Based on data by [40] and COST 259 [42], the AoDs for the different paths follow a uniform distribution with a fixed width of 80° centered at broadside of the antenna(s) at the BS. In addition, the individual path delays follow a uniform distribution between zero and 1.2 μ s, see Table I. Finally, the analysis of pathloss and shadowing is described in detail in Section III-B.

E. Generation of Wideband Parameters

In this section, the methodology of generating wideband parameters for each base-terminal link is presented. Its aim is to model the full wideband spatiotemporal channel response in a way that is both manageable from a complexity point of view and also quantitatively in agreement with measured properties of the channel, as described previously. Thus, a fixed number of paths N = 6, with distinct delays is generated, each with its own delay and mean AoD and AoA, consistent with the measured statistics. These N paths have a different interpretation in the macrocell and microcell environments, and thus these two cases will be treated separately below. In the former, the N paths collectively represent a single cluster of paths, leading to relatively small angular distances at the base. In contrast, in the latter case the N paths represent N distinct clusters, with large relative angular distances at the base.

1) Urban Macrocell and Suburban Macrocell: Starting with the macrocell environments, we need to generate the characteristics of each of the N paths, namely their delays, power, and mean AoD and AoA.

Path delays: The random delays of the paths have been seen experimentally to follow an approximate exponential distribution [45]. Thus, they can be expressed as

$$\tau'_n = -r_{\rm DS}\sigma_{\rm DS}\ln z_n, \qquad n = 1,\dots,N \tag{9}$$

where $z_n(n = 1, ..., N)$ are independent identically distributed (i.i.d.) random variables with uniform distribution U(0, 1)and $\sigma_{\rm DS}$ is derived in Section II-D. It should be emphasized that the time-scale for the generation of the delays τ'_n is generally not the same as that of the power delay profile (PDP) given by $\sigma_{\rm DS}$ (and hence $r_{\rm DS}$, signifying the ratio of the two time constants is not equal to unity). While $\sigma_{\rm DS}$ is related to the power density as a function of delay, $r_{\rm DS}\sigma_{\rm DS}$ is the nonpower weighted time-constant and, therefore, should be larger than $\sigma_{\rm DS}$, since the first paths usually have more power, and thus, the power-weighted time spread is smaller than the nonpower-weighted one [45]. For simplicity, $r_{\rm DS}$ is chosen to be a constant, independent of the particular realization of $\sigma_{\rm DS}$. Its values are given in Table I.

The τ'_n variables are then ordered so that $\tau'_{(N)} > \tau'_{(N-1)} > \cdots > \tau'_{(1)}$. Then, their minimum is subtracted from all, i.e., $\tau_n = (\tau'_{(n)} - \tau'_{(1)})$, with $n = 1, \ldots, N$, so that $\tau_N > \cdots > \tau_1 = 0$.

Path powers: There is sufficient experimental evidence that the PDP has an approximate exponential distribution [30] and [45]. Thus, the average powers of the N paths can be expressed as

$$P'_{n} = e^{\frac{(1-r_{\rm DS})\tau_{n}}{r_{\rm DS}\cdot\sigma_{\rm DS}}} \cdot 10^{-0.1\xi_{n}} \qquad n = 1,\dots,N.$$
(10)

 ξ_n for n = 1, ..., N are i.i.d. Gaussian random variables with standard deviation $\sigma_{\text{RND}} = 3$ dB, signifying the fluctuations of the powers away from the average exponential behavior. This parameter is also necessary to produce a dynamic range comparable to measurements, see [46]. Average powers are then normalized, so that the total average power for all N paths is equal to unity

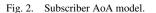
$$P_n = \frac{P'_n}{\sum_{j=1}^N P'_j}.$$
 (11)

Angles of Departure (AoD): The spatial character of the adopted channel has a relatively large (N = 6) number of paths, each with a small AS (set to 2° in the macrocell case). This model would be quite accurate in the limit of many paths $(N \gg 1)$, when the channel response approaches a continuum. For simplicity only N = 6 such paths are used. To satisfy the overall, composite AS of σ_{AS} described in the previous section, the distribution of AoD at the BS has to be specified. For simplicity, a Gaussian distribution with variance $\sigma_{AoD} = r_{AS}\sigma_{AS}$ is chosen. The value of the proportionality constant r_{AS} is close to the measured values in [45] and is given in Table I. Higher values of r_{AS} correspond to power being more concentrated in a small AoD or a small number of paths that are closely spaced in angle. Thus, the values of the AoD are initially given by

$$\delta_n' \sim N\left(0, \sigma_{\text{AoD}}^2\right) \tag{12}$$

where n = 1, ..., N. These variables are given in degrees and they are ordered in increasing absolute value so that $|\delta'_{(1)}| < |\delta'_{(2)}| < \cdots < |\delta'_{(N)}|$. The AoDs $\delta_{n,AoD}$, n = 1, ..., N are assigned to the ordered variables so that $\delta_{n,AoD} = \delta'_{(n)}$, n = 1, ..., N.

Angles of Arrival (AoA): Similar to the case of AoDs, a model is necessary for the statistics of the AoAs at the MS. In data collected in a suburban Chicago environment, [47], it was observed that the paths that come from or close to the LOS tend to have higher relative power. The measurements showed



that the AoA at the MS has a truncated normal distribution with mean zero with respect to the LOS, i.e.,

$$\delta_{n,\text{AoA}} \sim N\left(0,\sigma_{n,\text{AoA}}^2\right)$$
 (13)

with n = 1, ..., N. The variance of each path depends on the path's relative power. Based on the measured data, the variance $\sigma_{n,AoA}$ was found to depend on the relative power of that path as follows:

$$\sigma_{n,\text{AoA}} = 104.12^{\circ} \cdot (1 - \exp(0.2175 \cdot P_{n,\text{dBr}})). \quad (14)$$

The $\sigma_{n,AoA}$ represents the standard deviation of the noncircular AS and $P_{n,dBr} < 0$ is the relative power of the *n*th path, in dBr, with respect to total received power. Fig. 2 illustrates the curve fit for the distribution of AoA obtained using uniformly spaced bins of the received power.

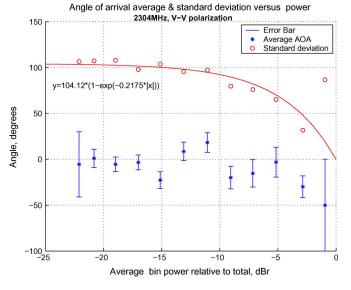
2) Urban Microcell: As discussed above, urban microcell environments differ from the macrocell environments in the way the paths are interpreted. In particular, since the individual multipaths correspond to separate clusters, they are independently shadowed. As in the macrocell case, N = 6 paths are modeled.

Path delays: Since the N paths correspond to independent multipath components, their delays τ_n , n = 1, ..., N are i.i.d. random variables drawn from a uniform distribution $U(0, 1.2 \,\mu\text{s})$ (see [42, Ch. 3.2.4]). The minimum of these delays is subtracted from all so that the first delay is zero. When the LOS model is used, the delay of the direct component will also be set equal to zero.

Path powers: The power of each of the N paths should depend on the delay of each path. As in the macrocell case, it is natural to make the dependence negative exponential (see [42, Ch. 3.2.4]), i.e.,

$$P'_{n} = 10^{-(\tau_{n}+0.1z_{n})} \tag{15}$$

where τ_n are the delays of each path in units of microseconds, and z_n (n = 1, ..., N) are i.i.d. zero-mean Gaussian random



variables with a standard deviation of 3 dB. Average powers are normalized so that total average power for all N paths is equal to unity. When the LOS model is used, the normalization of the path powers has to include the power of the direct component $P_{\rm D}$ so that the ratio of powers in the direct path to the scattered paths is equal to K

$$P_n = \frac{P'_n}{(K+1)\sum_{j=1}^N P'_j}, \qquad P_{\rm D} = \frac{K}{K+1}.$$
 (16)

Note that in the real world, a non-zero K-factor can be encountered even in channels that are NLOS. This would be the case when a dominant component is present. The default model here assumes the presence of Rayleigh fading only when not in LOS conditions.

AoD: In the microcell case, each of the N paths is assumed to arrive from independent directions. As a result, their AoD at the base can be modeled as i.i.d. uniformly distributed random variables. For simplicity, the width of the distribution is kept finite, between -40° to $+40^{\circ}$

$$\delta_{n,\text{AoD}} \sim U(-40^\circ, +40^\circ) \tag{17}$$

where n = 1, ..., N. One can now associate a power to each of the path delays determined above. Note that, unlike the macrocell environment, the AoDs do not need to be sorted before being assigned to a path power. When the LOS model is used, the AoD for the direct component is set equal to the LOS path direction.

AoA: The mean AoA of each path can be determined similar to the way discussed in the macrocell case. In this case, the AoAs are i.i.d Gaussian random variables

$$\delta_{n,\text{AoA}} \sim N(0, \sigma_{n,\text{AoA}}^2), \quad \text{where } n = 1, \dots, N \quad (18)$$

$$\sigma_{n,\text{AoA}} = 104.12^{\circ} \left[1 - \exp(0.265 \cdot P_{\text{dBr}}) \right]$$
(19)

and $P_{\rm dBr}$ is the relative power of the *n*th path in dBr. When the LOS model is used, the AoA for the direct component is set equal to the LOS path direction.

F. Generation of Fast-Fading Coefficients

The methodology developed previously will now be extended for the generation of fast fading coefficients for wideband time-varying MIMO channels with S transmit antennas and U receive antennas. The fast-fading coefficients for each of the N paths are constructed by the superposition of M individual subpaths, where each is modeled as a wave component. The mth component (m = 1, ..., M) is characterized by a relative angular offset to the mean AoD of the path at the BS, a relative angular offset to the mean AoA at the MS, a power and an overall phase. M is fixed to M = 20, and all subpaths have the same power P_n/M . The subpath delays are identical and equal to their corresponding path's delay. This simplification is necessary since the model has a limited delay resolution. The overall phase of each subpath $\Phi_{n,m}$ is i.i.d. and drawn from a uniform $[0, 2\pi)$ distribution. The relative offset of the *m*th subpath $\Delta_{n,m,AoD}$ at the BS, and $\Delta_{n,m,AoA}$ at the MS take fixed values given in Table II. For example, for the urban and

TABLE II SUBPATH AOD AND AOA OFFSETS

| Sub- | Offset at BS, | Offset at BS | Offset at MS |
|--------|--------------------|--------------------|--------------------|
| path | $AS = 2^{\circ},$ | $AS = 5^{\circ}$ | $AS = 35^{\circ}$ |
| number | Macrocell | Microcell | |
| (m) | $\Delta_{n,m,AoD}$ | $\Delta_{n,m,AoD}$ | $\Delta_{n,m,AoA}$ |
| | (degrees) | (degrees) | (degrees) |
| 1, 2 | ± 0.0894 | ± 0.2236 | ± 1.5649 |
| 3, 4 | ± 0.2826 | ± 0.7064 | ± 4.9447 |
| 5, 6 | ± 0.4984 | ± 1.2461 | ± 8.7224 |
| 7, 8 | ± 0.7431 | ± 1.8578 | ± 13.0045 |
| 9, 10 | ± 1.0257 | ± 2.5642 | ± 17.9492 |
| 11, 12 | ± 1.3594 | ± 3.3986 | ± 23.7899 |
| 13, 14 | ± 1.7688 | ± 4.4220 | ± 30.9538 |
| 15, 16 | ± 2.2961 | ± 5.7403 | ± 40.1824 |
| 17, 18 | ± 3.0389 | ± 7.5974 | ± 53.1816 |
| 19, 20 | ± 4.3101 | ± 10.7753 | ± 75.4274 |

suburban macrocell cases, the offsets for the first and second subpaths at the BS are, respectively, $\Delta_{n,1,AoD} = 0.0894^{\circ}$ and $\Delta_{n,2,AoD} = -0.0894^{\circ}$. These offsets are chosen to result to the desired fixed per-path ASs (2° for the macrocell environments, 5° for the microcell environment for $\Delta_{n,m,AoD}$ at the BS and 35° at the MS for $\Delta_{n,m,AoA}$). These per-path ASs should not be confused with the composite AS σ_{AS} of the composite signal with N paths.

It is also required that the BS and MS subpaths are associated, by connecting their respective parameters. While the *n*th BS path (defined by its delay τ_n , power P_n , and AoD $\delta_{n,AoD}$) is uniquely associated with the *n*th MS path (defined by its AoA $\delta_{n,AoA}$) because of the ordering, an explicit procedure must be defined for the subpaths. It is thus proposed that for the *n*th path, randomly pair each of the *M* BS subpaths (defined by its offset $\Delta_{n,m,AoD}$) with an MS subpath (defined by its offset $\Delta_{n,m,AoA}$). Each subpath pair is combined and the phases defined by $\Phi_{n,m}$ are applied. To simplify the notation, a renumbering of the *M* MS subpath offsets with their newly associated BS subpath is done. In other words, if the first (m = 1)BS subpath is randomly paired with the tenth (m = 10)MS subpath, then re associate $\Delta_{n,1,AoA}$ (after pairing) with $\Delta_{n,10,AoA}$ (before pairing).

Summarizing, for the nth path, the AoD of the mth subpath is

$$\theta_{n,m,\text{AoD}} = \theta_{\text{BS}} + \delta_{n,\text{AoD}} + \Delta_{n,m,\text{AoD}}$$
(20)

from the BS array broadside. Similarly, the AoA of the mth subpath for the nth path (from the MS array broadside) is

$$\theta_{n,m,\text{AoA}} = \theta_{\text{MS}} + \delta_{n,\text{AoA}} + \Delta_{n,m,\text{AoA}}$$
(21)

The antenna gains are dependent on these subpath AoDs and AoAs. For the BS and MS, these are given, respectively, as $|\chi_{\text{BS}}(\theta_{n,m,\text{AoD}})|^2$ and $|\chi_{\text{MS}}(\theta_{n,m,\text{AoA}})|^2$, where $\chi(\theta)$ is the corresponding complex antenna response to and from radiation with angle θ .

Last, the path loss (PL in linear scale), based on the BS to MS distance and the log-normal shadow fading, generated as described in Section II-E are applied to each of the subpath powers of the channel model.

The channel transfer function between receiver u and transmitter s at path n and time t is determined by the superposition of a large number of sinusoidal subpaths [35] as follows:

$$h_{u,s,n}(t) = \sqrt{\frac{P_n \sigma_{\rm SF} PL}{M}} \\ \times \sum_{m=1}^{M} \left(e^{jk \|\mathbf{v}\| \cos(\theta_{n,m,\rm AoA} - \theta_v)t} \chi_{\rm BS}(\theta_{n,m,\rm AoD}) \right) \\ \cdot e^{j(kd_s \sin(\theta_{n,m,\rm AoD}) + \Phi_{n,m})} \chi_{\rm MS}(\theta_{n,m,\rm AoA}) \\ \cdot e^{jkd_u \sin(\theta_{n,m,\rm AoA})} \right)$$
(22)

where in addition to the earlier definitions, the following hold.

- k wavenumber $2\pi/\lambda$ where λ is the carrier wavelength in meters;
- d_s distance in meters of the BS antenna element s from the reference (s = 1) element. For the reference element $s = 1, d_1 = 0;$
- d_u distance in meters of the MS antenna element u from the reference (u = 1) element. For the reference element $u = 1, d_1 = 0.$

Equation (22) provides a simple expression to generate a timedependent $U \times S$ channel matrix $\mathbf{H}(t)$ for a wideband MIMO system.

Measurements have shown that the elevation spread at the BS is much less than the azimuthal spread, [42]. For simplicity, this dependence is not included here. As mentioned in Section II, all channel parameters in (22) are time-varying at different time scales. The large-scale parameters, including power azimuth spectrum (PAS), PDP, AoD, and AoA, are updated in each run of the simulation drop. The positional vector of the mobile is varying at the speed of the mobile, which leads to rapid phase changes in the subpaths and the small-scale fading of the combined signal. It is also worth mentioning that the model's structure is flexible to include joint distribution of PDP and PAS, but has not been considered in this paper. In fact, the PAS in (22), as well as the AoA and AoD can be functions of delay.

III. ADDITIONAL OPTIONS

Beyond the main categorization of channels utilized in the previous sections, often some special channel environments occur that cannot be adequately described with the abovedeveloped models. Four additional special-case channel types are analyzed below and respective models are developed for each.

A. Far Scatterer Clusters

Signals arrive at the BS not only from the (approximate) direction of the MS, but also from other, separate regions of the delay/azimuth plane. These contributions correspond to radiation that is reflected or scattered at mountains, high-rise buildings, and other distinct geographical and morphological structures. This effect has been observed in many measurements, especially metropolitan areas that either have several high-rise buildings (published measurements collected in Frankfurt, Germany [48], [49]; Paris, France [50]; and

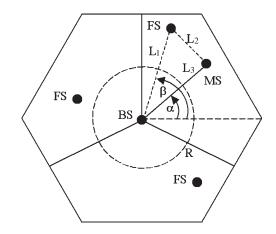


Fig. 3. Far-scattering cluster geometry.

San Francisco, CA [51]), or urban areas with interspersed unbuilt-up areas (e.g., Stockholm, Sweden [52]). The high-rise buildings can act either as specular reflectors, or as diffuse scatterers, depending on the building surface. In the following, the term "scatterers" will be used without loss of generality.¹ For microcell environments, the propagation processes leading to far scatterers are somewhat different, where waves travel from the transmitter to the receiver via waveguiding. Different waveguides thus give rise to different clusters due to different propagation times and/or angles of incidence at the transmitter and receiver. The far scatterers lead to an increase of the angular spread as well as the DS of the arriving signal. It has been shown, e.g., in [53], that this leads to important changes in MIMO channel characteristics. Thus, far scatterer clusters are included as an option for this model.

The far scattering cluster (FSC) model presented here is a simplified model easily implemented in a system simulator, and containing the necessary elements to reproduce the key effects of the FSC. The model inserts three FSCs in the cell area covered by each BS. Each FSC is then positioned randomly across the hexagonal area of service of the BS following the uniform distribution. The positioning process also imposes the constraint of the FSC being at least R = 500 m from the BS. Only the FSC that is closest to each MS is selected to be visible to that MS while the other FSCs in the cell are not present in the formation of that MS's channel model. The visible FSC then contributes paths to the MS's channel model, in addition to the default paths produced by the scattering around the MS. This approach makes use of FSCs in adjacent sectors when they are closer to the mobile than an FSCs in the serving BS. In this model, the three far-scatterers are independent of the BS antenna configuration or the number of sectors. The geometry shown in Fig. 3 is used to define several of the model parameters. The composite base AS associated with the NLOS propagation model will have an average AoD in the direction of α , and the individual path AoDs are simulated as in the urban macrocell model. For the geometry defined by the FS, two of the N multipath components are associated with the path to the FS, having a mean angle β , determined by the geometry of the FS location. Similarly, the path delays are defined by the

¹The more precise term "interacting objects" is used in [64].

distances, $L_1 + L_2$, the path distance from BS to MS via the FS, and L_3 , the shortest path from BS to MS. The delays are specified by $\tau_{\text{primary}} = L_3/c_0$, and $\tau_{\text{excess}} = (L_1 + L_2 - L_3)/c_0$, where c_0 is the speed of light. The path delays and relative angles are chosen in the same way as for the primary path.

To implement the FSC model, the macrocell channel model described in previous sections is modified by applying the calculated excess delay and path loss to the two late arriving paths. The additional path loss of $1 \text{ dB}/\mu s$ is added with a 10 dB maximum [32]. Before normalizing the path powers to unity, a site-correlated log-normal shadowing 8 dB/ $\sqrt{2}$ is applied to the two groups of multipaths associated with the primary path and excess path as defined above. The shadow fading has been observed to be common among paths of the same cluster, and different between clusters. A site-to-site correlation is used in this case since the environmental characteristics near the mobile are common to both paths producing correlated shadowing. A 50% correlation is assumed resulting in half the variance observed per cluster, i.e., the square root of two. After normalizing the path powers to unity, a final step of applying a common log-normal shadowing random coefficient to all paths is performed similar to the macrocell model.

When the far scatterer is added to the model with its extra path length, the DS is increased accordingly. The average value increases from the 0.65 μ s for the No-FS case to 0.98 μ s for the FS case. There is also an increased average AS caused by the relative angle difference and the powers associated with the signals arriving from the later cluster, e.g., the nominal AS = 15° increases to 22.9°.

B. Microcell LOS Modeling

LOS paths occur when a direct "unobstructed" path exists between the base and subscriber. For microcells, LOS paths are typically present in combination with additional reflected paths producing canyon effects as described by the COST-Walfish–Ikegami street canyon model [37]. This model results in a propagation slope modified from an ideal LOS path with an exponent of 2.0 to an exponent of 2.6, which is an empirical result based on measurements. LOS paths typically occur with greater probability when the subscriber is close to the base, where the path is more likely to be free of obstructions. At larger distances LOS conditions are typically more rare. These relationships are captured in the probability of occurrence of an LOS condition [30]

Prob. of LOS =
$$\frac{300 - d}{300}$$
, for d (in meters) < 300 m. (23)

The microcell LOS model adds an additional LOS component, which is scaled in proportion to the scattered multipath components to result in a K-factor, set [54] by

If (LOS) :
$$K = 13.0 - 0.03 \cdot d$$
, K in decibels, $d < 300$ m
If (NLOS) : $K = -\infty$ dB. (24)

When the LOS condition is selected, the Walfish–Ikegami street canyon model [37] is used as the propagation loss model,

with the simplified equation as specified in (3). A log-normal shadow fading $\sigma_{SF} = 4 \text{ dB}$ is chosen to represent the variations seen in the LOS street canyon environment.

When the NLOS condition is present, the Walfish–Ikegami microcell model [37] is selected, with some simplifications (for a typical street environment and average angle of propagation), as described in (2). The log-normal shadow fading is 10 dB for the NLOS path loss model.

By including an LOS path in the model, a reduction in average AS and average DS is produced since the stronger direct component occurs at zero degrees and zero delay with respect to the MS. In addition, significantly more of the lower values of AS and DS (after the addition of the LOS component) occur than for the strictly NLOS case. These low values represent cases that are more highly correlated.

C. Urban Canyon Modeling

Street canyon effects, consisting of several propagation mechanisms can be found in dense urban areas where signals propagate between building rows. In canyons, received signals typically contain multiple delayed paths arriving from similar angles and having narrow ASs. Environment-specific effects are evident [50], with some locations having first arriving paths from overrooftop propagation and later paths arriving from down the street. In other locations, down the street paths are the dominant effect, where path AoAs are all similar. Since these effects vary with location, a simplified model was created to simulate urban canyon effects without the need for defining building grids.

When the paths arriving at the subscriber are confined to a narrow set of AoAs, the correlation between subscriber antennas is typically at its highest. This is an important situation to test in a multiantenna study. To emulate the canyon effect, a channel generating parameter α is defined and used to set the probability of obtaining all paths coincident in angle of arrival at the subscriber. The value of α was selected to be 90% as a preferred value to emphasize the occurrence of the common angle of arrival. For the remaining 10%, the standard power dependent angle of arrival model is used at the subscriber. This model will produce composite AS = 35° (the per-path AS) with a 90% occurrence, and for the remaining 10% a value ranging from 35° to about 100°.

D. Polarization Propagation: Modeling and Parameters

Usually, channel models analyze only the propagation of vertical polarization, corresponding to the transmission and reception from vertically polarized antennas. Recently, antenna architectures with cross-polarized antennas have been considered. Therefore, it is necessary to model the propagation and mixing of dual-polarized radiation. To be consistent with previous models, only propagation in the two-dimensional (horizontal) plane will be considered. Therefore, it is natural to split the radiation into two components, namely vertically and horizontally polarized radiation. The transmission from a vertically polarized antenna will undergo scattering resulting to energy leaked into the horizontal polarization before reaching the receiver antenna. By employing two colocated antennas at the receiver with orthogonal polarizations the total received signal power will be higher from that of a single vertically polarized antenna.

In the remainder of the section, polarized antennas will be defined as structures that receive or transmit at one polarization. Whatever the implementation of a polarized antenna might be, the definitions and modeling to follow will assume that an equivalent response on a 2-D plane can be defined, which can be fully characterized by its decomposition into the two orthogonal axes: vertical, (V), and horizontal, (H). Polarized antennas will be used for transmission or reception at the BS or at the MS.

The channel phenomena appearing in multipolarization transmission can be categorized in three areas.

- 1) PDP: The PDP can be analyzed on a per path and polarization basis. The delays of two polarizations for a given path coincide in time. The average path powers of the horizontal and vertical polarizations assuming the transmission from, e.g., a vertically polarized antenna are generally unequal. [55]–[58]. The cross-polarizationdiscrimination (XPD), is a typical figure of merit used in characterizing the mean power transfer from one polarization to another. It is defined as $XPD = P_{V-V}/P_{V-H}$, which assumes that the transmission originates in the V polarization and the receiver observes power P_{V-V} in the V orientation versus P_{V-H} in the H orientation. Also, XPD is not necessarily identical between paths. Statistical descriptions on the variability of the XPD between paths has been reported and will be used here.
- 2) Spatial Profile: When comparing the per path spatial behavior between two polarizations, there is no conclusive studies that show in what manner they could be different. Thus, in the absence of any data, the rms per path AS and the mean per path AoD/AoA are assumed to be identical for the respective paths between the two polarizations.
- 3) Symmetry: No conclusive studies exist supporting that the H originated transmission should have different statistics than the V one. Thus, for simplicity it is assumed that the two types of coupling exhibit identical XPD statistics while having independent XPD instantiations for each polarization.

1) Polarization Measurement Data: The polarization measurements available in the literature can be categorized by the type of environment in which they were obtained. Macrocells tend to exhibit different XPD statistics (i.e., first- and secondorder moments) than microcells due to the significant difference in the amount of scattering, [59]. Although XPD models have been proposed based on semianalytical approach, such as in [60], here the effort is to base the model on measurement data. The XPD was measured in the same measurement campaign as the angle-of-arrival in the Chicago suburbs (Schaumburg), [61], using V and H polarized antennas at both ends. Fig. 4 describes the ratios of P_{V-V}/P_{V-H} , and P_{V-V}/P_{H-V} . The XPD shows a linear dependence with path power with a 5.2-dB standard deviation with respect to the linear regression. As seen in Fig. 4, the median value of XPD is dependent on the mean relative power of the measured path. For example, if the power is confined to a single path, i.e., 0 dBr, the median

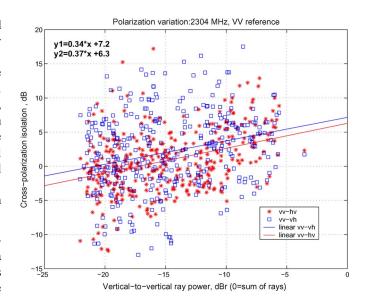


Fig. 4. XPD versus path (ray) power.

XPD is approximately 7 dB. For weaker paths, e.g., -20 dBr, the median XPD is approximately 0 dB. During its propagation an electromagnetic wave (ray) would suffer several parallel and oblique reflections, and diffractions that change its polarization and decrease its power. One expects that the more scattering a wave suffers, the more mixing its polarization will undergo and the weaker its power will become. Therefore, it is expected that both the XPD and the wave power will decrease considerably after a number of random reflections. For modeling purposes XPD random realizations, independent for each path, are drawn for urban macrocell and microcell, as

$$P_{V-H} = P_{V-V} + A + B \cdot N(0, 1) \tag{25}$$

Urban Macro : $A = 0.34P_{n \text{ dB}} + 7.2 \text{ dB}, \qquad B = 5.5 \text{ dB}$

Urban Micro : A = 8 dB, B = 8 dB

where a V polarization is assumed for transmission, $P_{n_dB} < 0$ is the mean relative path Power P_n in dBr, and B corresponds to the lognormal standard deviation of the XPD draw.

2) Channel Coefficients for Polarized Antennas: An extension to the model in Section II-F is defined

$$h_{u,s,n}(t) = \sqrt{\frac{P_n \sigma_{\rm SF} PL}{M}} \\ \times \sum_{m=1}^{M} \left(\begin{bmatrix} \chi_{\rm BS}^v(\theta_{n,m,\rm AoD}) \\ \chi_{\rm BS}^h(\theta_{n,m,\rm AoD}) \end{bmatrix}^{\rm T} \\ \times \begin{bmatrix} e^{j\Phi_{n,m}^{(v,v)}} & \sqrt{r_{n1}}e^{j\Phi_{n,m}^{(h,v)}} \\ \sqrt{r_{n2}}e^{j\Phi_{n,m}^{(v,h)}} & e^{j\Phi_{n,m}^{(h,h)}} \end{bmatrix} \\ \times \begin{bmatrix} \chi_{\rm MS}^v(\theta_{n,m,\rm AoA}) \\ \chi_{\rm MS}^h(\theta_{n,m,\rm AoA}) \end{bmatrix} e^{jkd_s\sin(\theta_{n,m,\rm AoD})} \\ \times e^{jkd_u\sin(\theta_{n,m,\rm AoA})} \\ \times e^{jk\|\mathbf{v}\|\cos(\theta_{n,m,\rm AoA} - \theta_v)t} \right)$$
(26)

where

- $\chi^h_{\rm BS}(\cdot)$ BS complex antenna response in the *H* polarization. The squared norm of the antenna response $\|\chi(\cdot)\|^2$ is the real valued antenna gain. The other χ 's are defined similarly.
- r_{n1} Defined as the inverse of the random variable drawn from (25) for the *n*th path, $r_{n1} \stackrel{\Delta}{=} (1/\text{XPD})$. An independent XPD value is assigned for each path. The corresponding random variable for the (H-V)versus the (V-V) ratio is defined as r_{n2} .
- $\Phi_{n,m}^{(h,v)}$ Initial random phase of the *m*th subpath in the *n*th path that originates in the *H* direction and arrives in the *V* direction. Each initial phase is drawn independently under the assumption that the fast fading for each antenna and polarization pair combination is assumed independent of the others.

Equation (26) defines the channel realization between a pair of antennas. The antennas are elements positioned in some generic direction in a two-dimensional plane so that their responses can be decomposed into V and H. Thus, each antenna response is a 2 × 1 complex vector. The 2 × 2 matrix defines the coupling in terms of scattering phases and amplitudes of all four combinations of the two transmit and two receive decompositions. It should be stressed that the correlations between antennas resulting from this form of channel can no longer be written in the form of a Kronecker matrix product of correlations of the transmitter and receiver arrays. Instead, they can be written as sums of such matrix products, with each product representing the correlations for a certain mode (e.g., (V-H), (H-H), etc.).

IV. SIMULATED MODEL STATISTICS

The wideband model developed in Section II specifies also the system-wide spatiotemporal profile, beyond the point-topoint channel characterization. Thus, all resulting output statistics from the model are presented in terms of cumulative distribution functions. The illustration of the resulting composite rms DS for the three environments using the parameters of Table I are given in Fig. 5 along with the targeted cumulative distribution functions (CDFs) obtained from the measurements. Similarly, the same family of quantities for the composite rms AS observed at the base is shown in Fig. 6.

Also, MIMO performance is evaluated for different MIMO BS and MS configurations and different channel environments. Significant correlation is necessary before capacity is reduced from uncorrelated, random channel matrix results. Wideband $U \times S$ MIMO capacity for a Suburban macrocell, urban macrocell, and urban microcell environments are evaluated using the spatial channel model specified here. A simple case of beam-steering is also included to compare the performance of the multistream MIMO capacity metric to that of a single stream, which should perform well for correlated environments. For simplicity, and to minimize feedback information, the single stream is beamformed to the LOS angle of departure of the user $\theta_{\rm BS} = 0$.

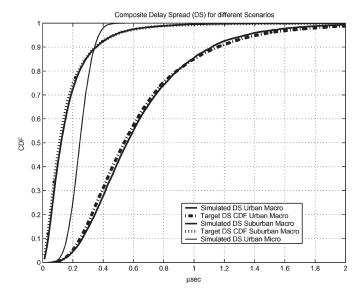


Fig. 5. Simulated and measured CDFs of DS for the three environments.

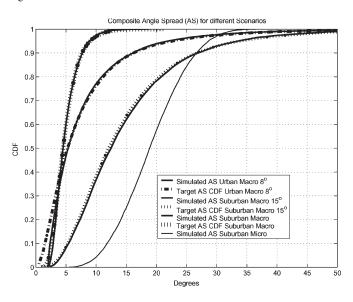


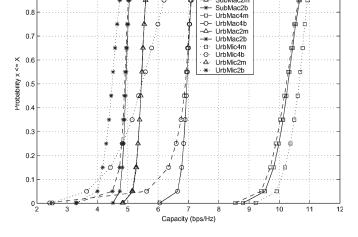
Fig. 6. Simulated and measured CDFs of AS for the three environments.

For the $U \times S$ channel matrix **H** the capacity C [22] is

$$C = \log_2 \left(\det \left[\mathbf{I} + \frac{\rho}{S} \mathbf{H} \mathbf{H}^{\dagger} \right] \right) \quad \text{b/s/Hz}$$
(27)

where I is a $U \times U$ identity matrix, \mathbf{H}^{\dagger} denotes transpose conjugate, and ρ is the average per-receiver-antenna signal-to-noise ratio (SNR).

The channel coefficients for each path are generated using the method in Section II-F, which produces MIMO channel matrices at different delays that are correlated both in time (Doppler spread) and space (antenna spacing) for each of the Nchannel paths. After superimposing all the six paths and sampling at a frequency ten times the maximum Doppler frequency, a discrete Fourier transform (DFT) is performed that results in the MIMO channel frequency response at each sample time. The wideband capacity can then be calculated in the frequency domain on a bin by bin basis by computing the average over the frequency bins. The average (over time) wideband capacity for



Average Capacity CDFs for SCM Channels 10 dB SNR

ó

O- SubMac4b

A SubMac2n

BubMac4m

Fig. 7. CDFs of average capacities for the three channel environments and four array configurations when SNR = 10 dB.

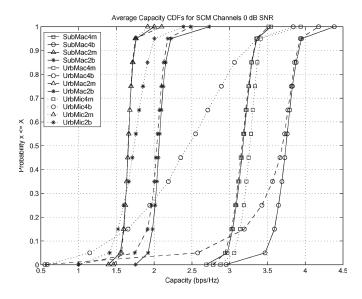


Fig. 8. CDFs of average capacities for the three channel environments and four array configurations when SNR = 0 dB.

each channel profile over a fading distance of 40λ is computed and the CDF of the 1000 channel profile average capacities is what is plotted. The equal transmit power MIMO capacity with S data streams is compared to the beamforming to broadside of a single data stream. For the composite case, the broadside beamforming capacity, which assumes approximate knowledge of the MS location), is given by

$$C = \log_2 \left(\det \left[\mathbf{I} + \frac{\rho}{S} \mathbf{H} \mathbf{v} \mathbf{v}^{\dagger} \mathbf{H}^{\dagger} \right] \right) \quad \text{b/s/Hz}$$
(28)

where **v** is an $S \times 1$ steering vector of all its elements equal to unity.

The results are shown in Figs. 7 and 8, with a uniform MS antenna spacing of 0.5λ . For the 4 × 4 configurations, the average MIMO capacity is shown when the BS antenna spacing is 4λ (SMac4m, UMac4m, and UMic4m), and the average broadside beamforming capacity is shown when the BS antenna

spacing is 0.5λ (SMac4b, UMac4b, and UMic4b). For the 2 × 2 configurations, the average MIMO capacity is shown when the BS antenna spacing is 10λ (SMac2m, UMac2m, and UMic2m), and the average broadside beamforming capacity is shown when the BS antenna spacing is 0.5λ (SMac2b, UMac2b, and UMic2b). At the low SNR, 0 dB, and for the channels with higher spatial correlation (macrocells), the beamforming techniques appear to be advantageous to the MIMO approach [62]. The BS antenna spacings in all MIMO configurations are chosen so that the total length of the uniform linear array is comparable in all cases.

Recall that the macroscopic and mesoscopic parameters are computed once for each user for a given simulation run. The only parameters that need to be computed for each channel realization are the fast-fading coefficients at the microscopic level. For a given multipath and transmit/receive antenna pair, these coefficients are generated by summing M = 20 sinusoids, and this computation comparable in complexity to the wellknown Jakes model [63] using M oscillators. The complexity of computing the complete MIMO channel per user for a large number of realizations is dominated by the computation of the fast-fading coefficients, and this complexity scales proportionally with NSU. For a large-scale simulation with many users over thousands of time instances, the total number of arithmetic operations required for computing the coefficients in on the order of millions; therefore, the complexity is easily manageable using any modern computer.

V. SUMMARY AND CONCLUSION

A unified spatiotemporal channel model framework was developed, which is applicable to multicell, system-level, simulations for up to 5 MHz bandwidth. Particularly, it describes the channel properties in three scales (macro-, meso-, and microscopic), and it specifies the dependencies between pathloss, temporal, and spatial physical parameters, their values, and the methods for implementing the model. It also provides modeling approaches for the special cases of far scatterer clusters, urban microcells, and urban canyon environments. The model also is extended to include the use of polarized antennas. While maintaining reasonable computational complexity, the model attempts to match the reported measurement data in the literature. Some examples of its output statistics are shown to illustrate the model's behavior.

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